

# **Semiconductor Lasers :** **Output Characteristics & SM Lasers**

**Bikash Nakarmi**

**Nanjing University of Aeronautics and Astronautics**

# OUTLINES

## **I. Output Characteristics of Laser**

- a. Threshold Current**
- b. Confinement Factor**
- c. Spatial Profile**
- d. Longitudinal modes**

## **II. Single Mode lasers**

- a. ECL**
- b. DFB & DBR lasers**
- c. VCSELs**
- d. Quantum Lasers**

# Basic Laser Theory

**Oscillator = Gain Medium + Feedback (Resonator)**

**Peak Gain coefficient:**  $\gamma_p = \alpha_a \left( \frac{\Delta n}{\Delta n_T} - 1 \right)$

**For steady state oscillation : Gain = Resonator loss**

**threshold peak Gain coefficient:**  $\gamma_{pt} = \alpha_r = \alpha_s + \frac{1}{2l} \ln \left( \frac{1}{R_1 R_2} \right)$

Typical Values:-

$$\alpha_s \approx 22 \text{ cm}^{-1}$$

$$l = 300 \mu\text{m}$$

$$\alpha_a \approx 600 \text{ cm}^{-1}$$

$$R_1 = R_2 = 0.32$$

$$\gamma_{pt} = 60 \text{ cm}^{-1}$$

# Basic theory

$$\gamma_p = \alpha_a \left( \frac{\Delta n}{\Delta n_T} - 1 \right)$$

$$\Rightarrow \left( \frac{\Delta n_t}{\Delta n_T} - 1 \right) = \frac{\gamma_p}{\alpha_a} = 0.1;$$

$$\frac{\Delta n_t}{\Delta n_T} = \frac{J_t}{J_T} = \frac{i_t}{i_T} = 1.1$$

$$\text{i.e. } i_t = 1.1 i_T$$

Temperature dependent of threshold current:-

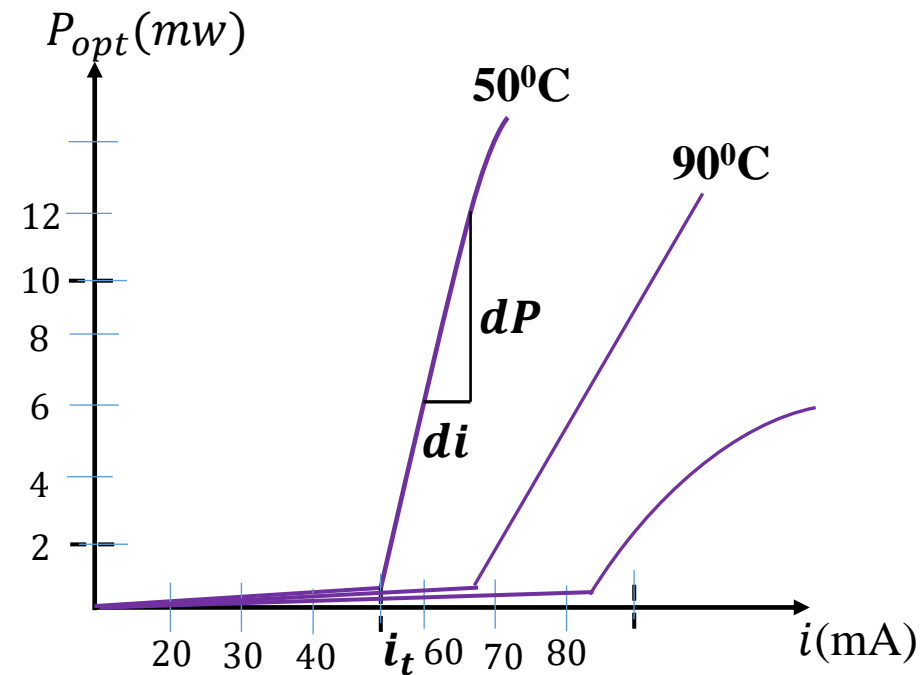
$$i_t(T) = i_0 e^{-T/T_0} \text{ (temperature characteristic)}$$

Above threshold:-

$$P_{opt} \propto (i - i_t)$$

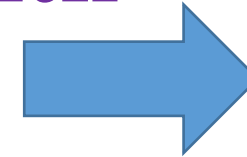
$$P_{opt} = k(i - i_t)$$

$$\frac{dP}{di} = \text{differential Responsivity (W/A)}$$

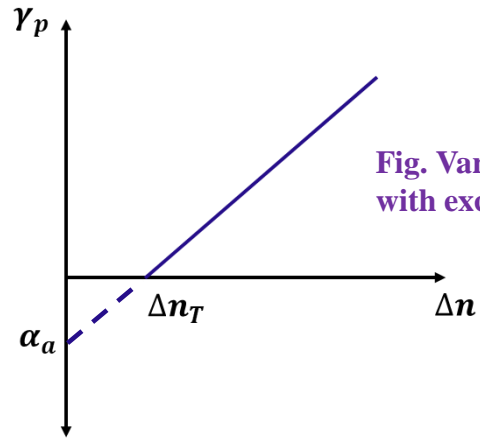


# Assignment # 2

**Why the threshold current increase with increase in the temperature?**



# Output Characteristics: **Threshold current**



$$\gamma_p = \alpha_a \left( \frac{\Delta n}{\Delta n_T} - 1 \right)$$

$$\Delta n = \alpha_a \left( \frac{(i/e)\tau}{l \times w \times d} \right) = \frac{J\tau}{ed}$$

$$\therefore J_T = \frac{\Delta ned}{\tau} \rightarrow J_T \propto d$$

**Laser Condition: Gain = Loss**

$$\gamma_{pt} = \alpha_r$$

$$\alpha_a \left( \frac{\Delta n_t}{\Delta n_T} - 1 \right) = \alpha_r$$

$$\alpha_r = \alpha_a \left( \frac{J_t}{J_T} - 1 \right)$$

$$\therefore J_t = J_T \left( 1 + \frac{\alpha_r}{\alpha_a} \right)$$

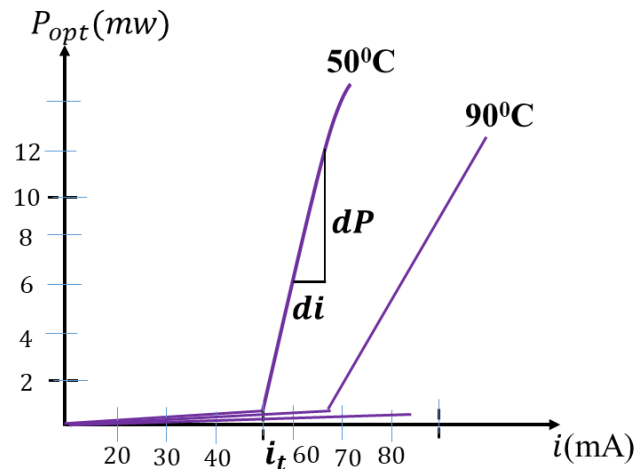
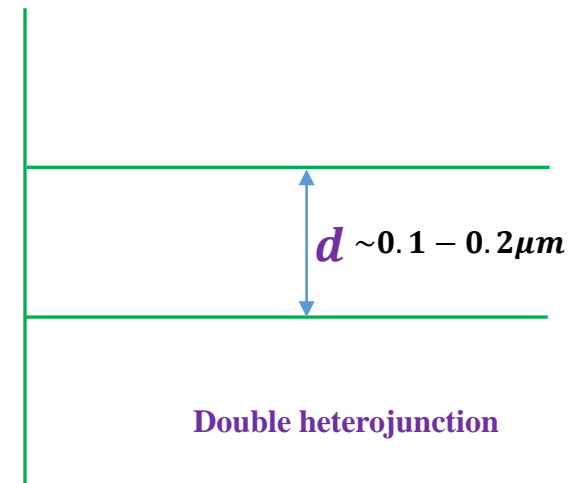
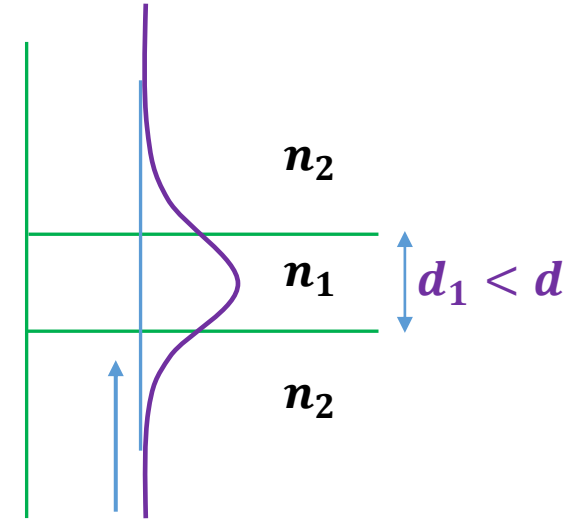
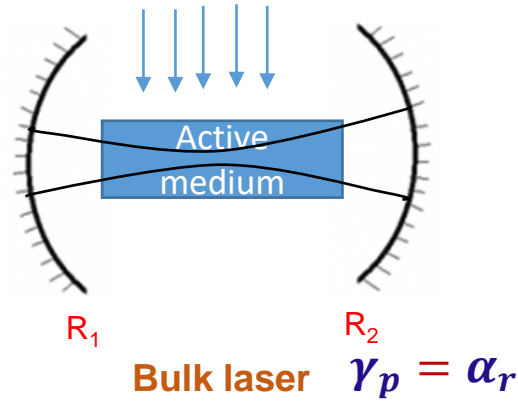
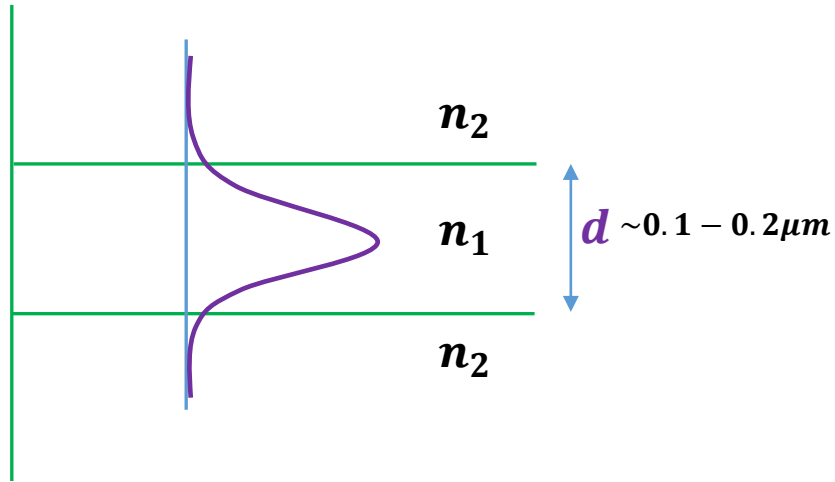


Fig. Threshold current variation with temperature



# Output Characteristics: **Confinement Factor, $\Gamma$**



**Confinement factor,  $\Gamma$**   $\rightarrow$  fractional energy in the active region

$$0 < \Gamma < 1$$

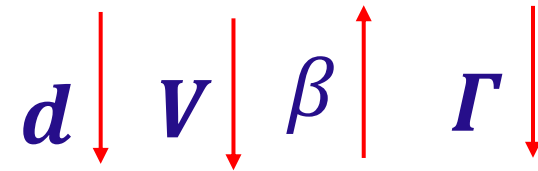
**cavity gain**  $= \Gamma \gamma_p$

$$\Gamma \gamma_p = \alpha_r = \Gamma \alpha_a \left( \frac{J_t}{J_T} - 1 \right)$$

$$\therefore J_t = J_T \left( 1 + \frac{\alpha_r}{\Gamma \alpha_a} \right)$$

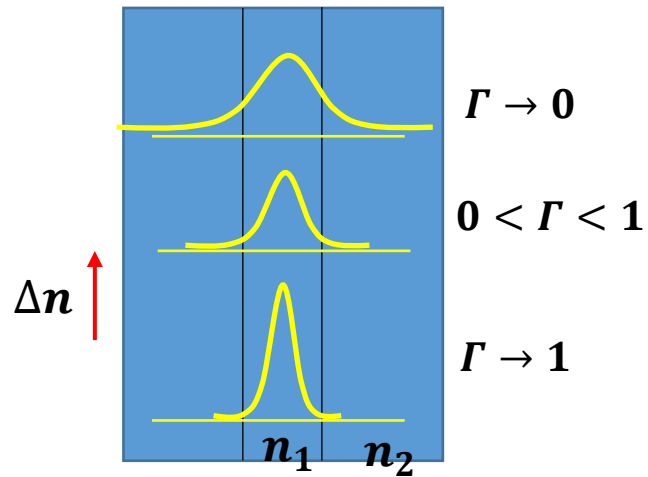
**V number,  $V = \frac{2\pi}{\lambda} d \sqrt{n_1^2 - n_2^2}$**

penetration depth,  $\frac{1}{\gamma} \rightarrow = 1 / \sqrt{\beta^2 - k_0^2 n_2^2}$

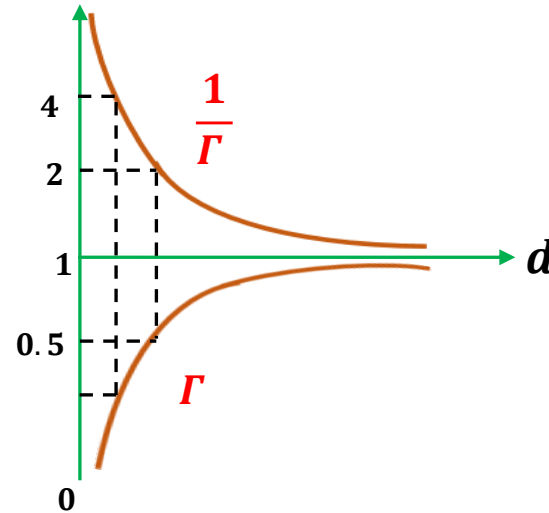


# Output Characteristics: Confinement Factor, $\Gamma$

V number,  $V = \frac{2\pi}{\lambda} d \sqrt{n_1^2 - n_2^2}$



$\Delta n = (n_1 - n_2)$  ↑ Tightly confined



$d$  decreases  $\Gamma$  becomes small ;  $\frac{1}{\Gamma}$  becomes large

$$J_t = J_T \left( 1 + \frac{\alpha_r}{\Gamma \alpha_a} \right)$$

$$= J_T + \left( \frac{\alpha_r}{\Gamma \alpha_a} \right) J_T$$

most practical value of  $\Gamma$  varies from 0.6 to 0.9

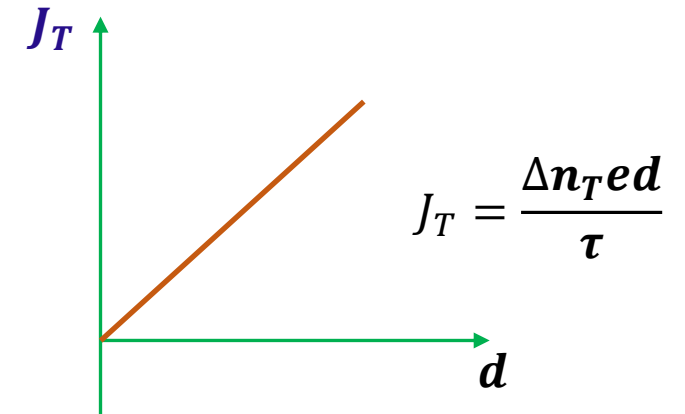


Fig. transparent current dependence on width of active region

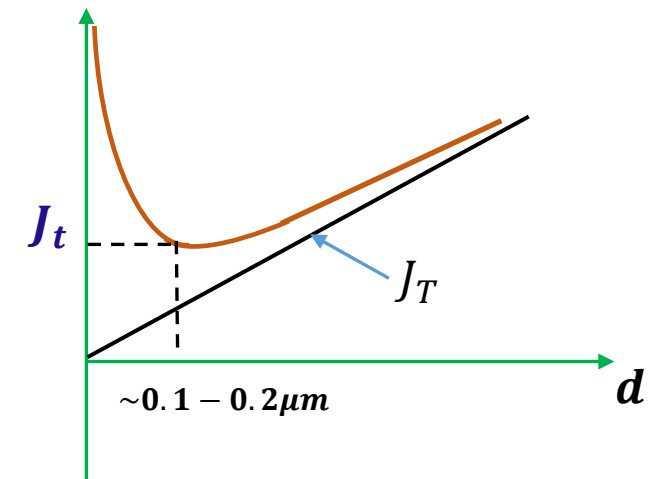
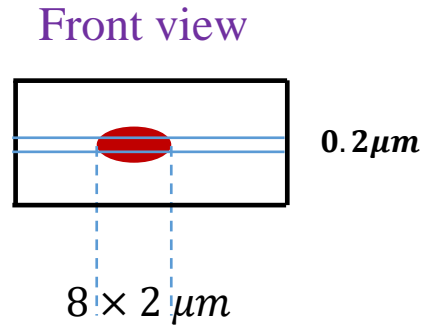
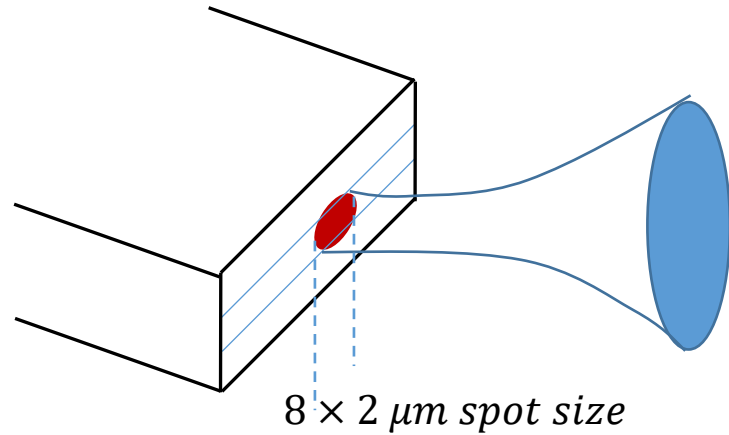


Fig. threshold current w.r.t. width of active region



# Output Characteristics: **Spatial Profile**

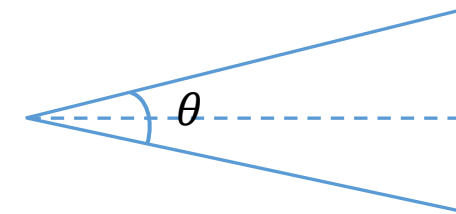


Example:-

$$\lambda = 1 \mu\text{m}$$

$$\theta_{\perp} \approx \sin^{-1} \left( \frac{\lambda}{d = 2} \right) = 30^{\circ}$$

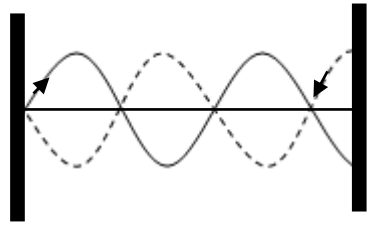
In 2D plane:



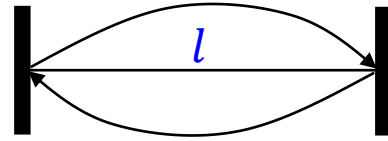
$$\theta_{\parallel} \approx \frac{\lambda}{d} \approx \frac{1}{8}$$

$$\theta_{\parallel} \approx 7^{\circ}$$

# Output Characteristics: Longitudinal Modes



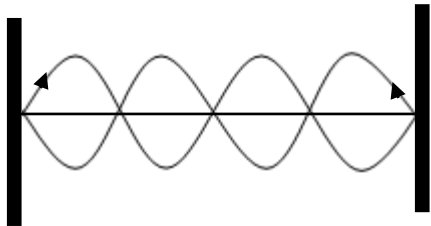
(a) FP resonator with arbitrary wave



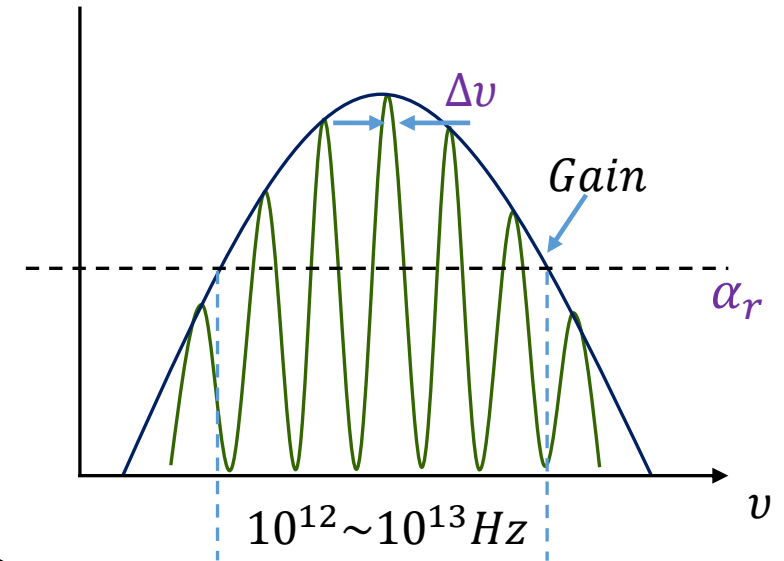
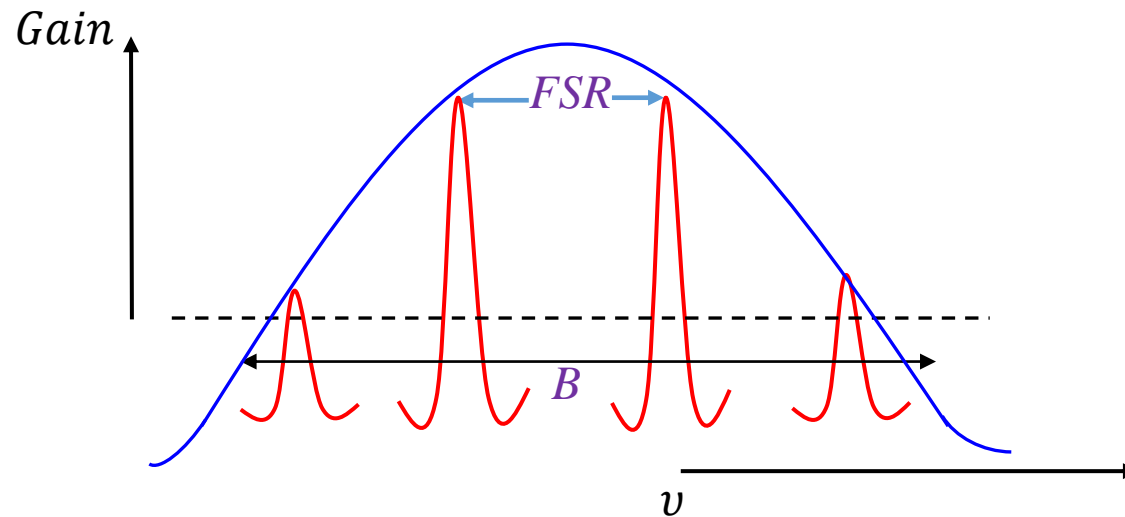
$$B \sim 10^{12} \text{ Hz}$$

$$\nu_F = \frac{c}{2nl} = \frac{3 \times 10^8}{2 \times 300 \times 10^{-6} \times 3.6} \approx 1.4 \times 10^{11} \text{ Hz}$$

$\Rightarrow$  few/several longitudinal modes =  $B/\nu_F$



(b) FP resonator with standing wave



**MODE SELECTION: ECL, DFB, DBR LASER**

# Output Characteristics: **Spectral linewidth**

$\Delta\lambda \rightarrow$  linewidth

**Typical:-**

$\Delta\lambda \sim 20 - 40$  nm for LED  
 $\sim 2 - 3$  nm for FP lasers  
 $\leq 0.1$  nm for DFB lasers, VCSELS

**Equivalence:-**

$$\Delta\lambda \leftrightarrow \Delta\nu$$

$$c = \nu\lambda \Rightarrow \nu = \frac{c}{\lambda}$$

$$\Delta\nu = \frac{c}{\lambda^2} (-\Delta\lambda)$$

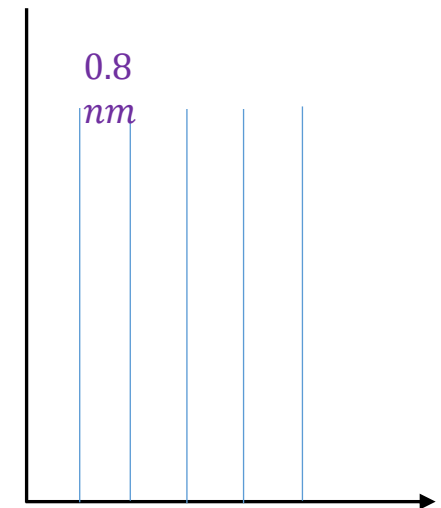
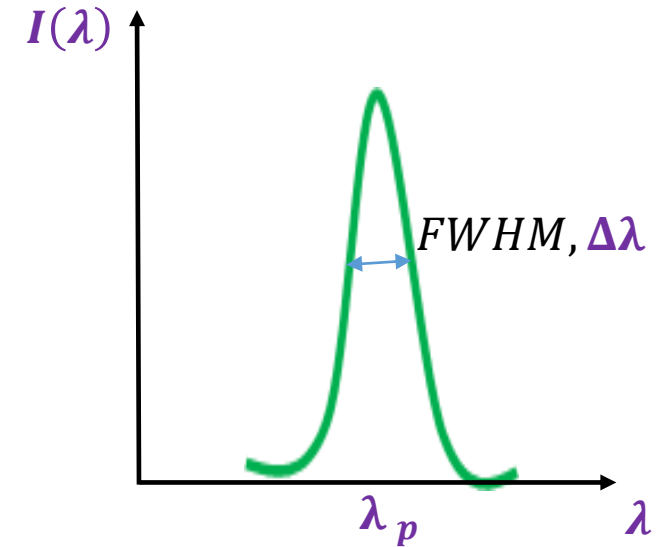
**For example:-**

$$\lambda = 1.55 \mu\text{m}$$

$$\Delta\lambda = 1 \text{ nm} \Rightarrow \Delta\nu = 125 \text{ GHz}$$

$$\Delta\nu = 100 \text{ GHz} \Rightarrow \Delta\lambda = 0.80 \text{ nm}$$

$$\Delta\nu = 100 \text{ MHz} \Rightarrow \Delta\lambda = 0.00080 \text{ nm}$$



# Output Characteristics: **Spectral linewidth**

## Importance of Narrow linewidth

### In DWDM

$\Delta\lambda(\text{source linewidth}) \ll \delta\lambda(\text{channel spacing})$

For 100 GHz channel spacing:  $\delta\lambda = 0.8 \text{ nm}$

For 50 GHz channel spacing :  $\delta\lambda = 0.4 \text{ nm}$

**$\Rightarrow \Delta\lambda < 0.1 \text{ nm}$  or smaller for no channel overlap**

### Dispersion in fiber link

Dispersion parameter:  $D = \frac{\Delta\tau}{L\Delta\lambda} \text{ ps/km-nm GHz}$

$\Delta\tau$  : Temporal spread of a pulse

$L$ : length of the link

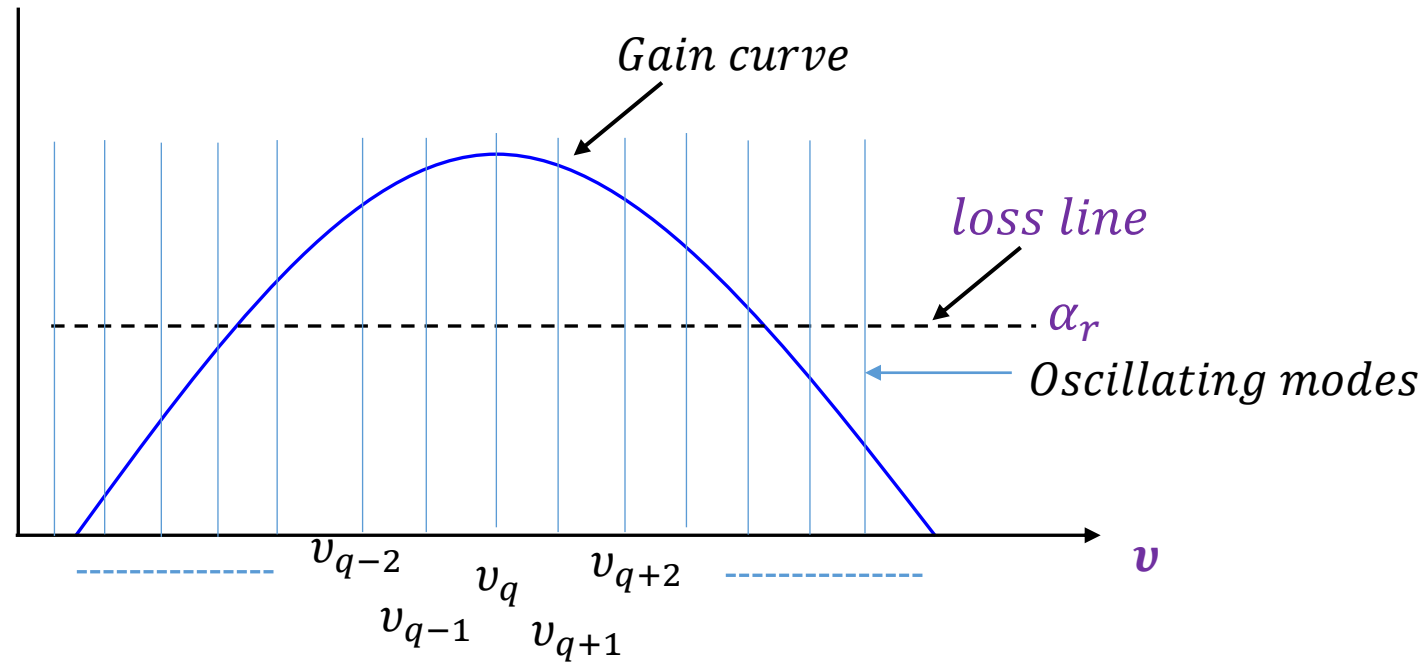
$\Delta\lambda$  : Source Linewidth

$$\Rightarrow \Delta\tau = D \times L \times \Delta\lambda$$

**$\Rightarrow$  smaller the  $\Delta\lambda$ , smaller is the spreading of the pulse,  $\Delta\tau$**

**$\Rightarrow$  larger bit rates are possible without ISI**

# Output Characteristics: multi-longitudinal mode oscillation

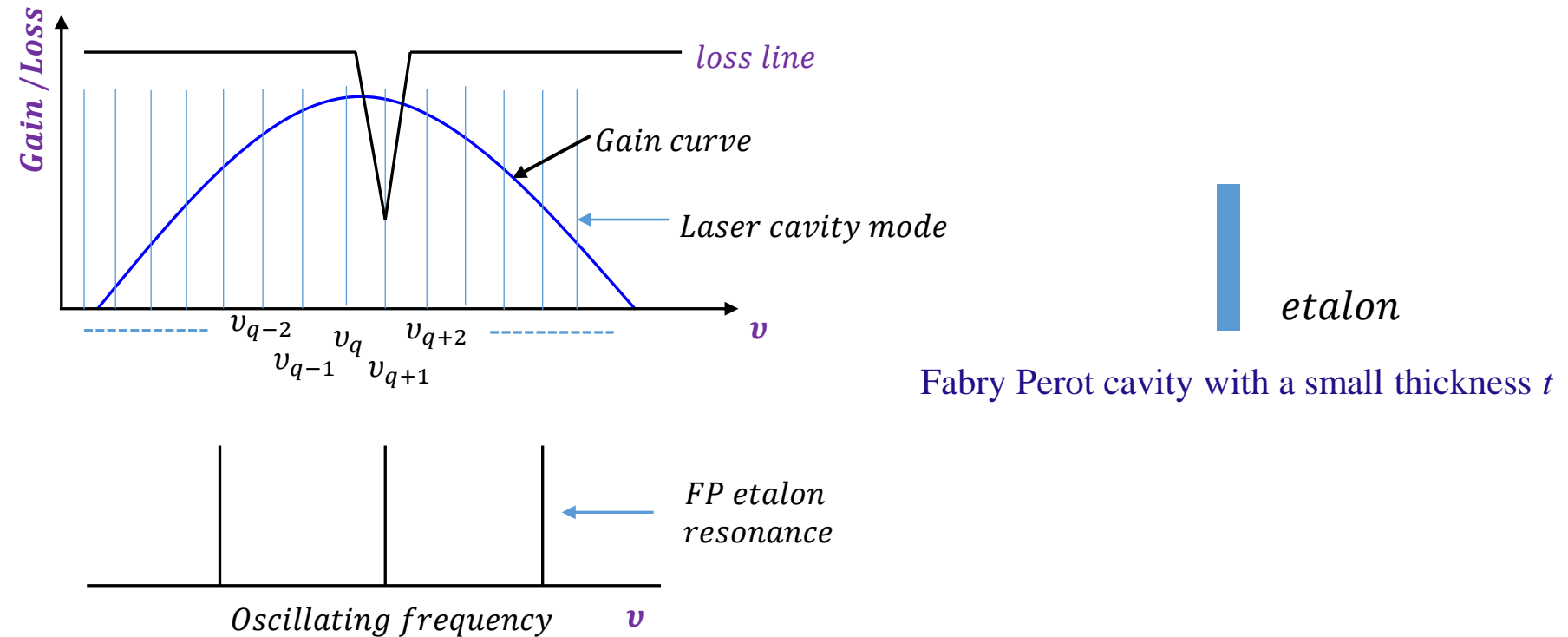


*Those modes which have gain more than loss will be able to oscillate leading to multi – frequency oscillation.*

**In the figure shown above, oscillation will occur at *Eight* frequencies**

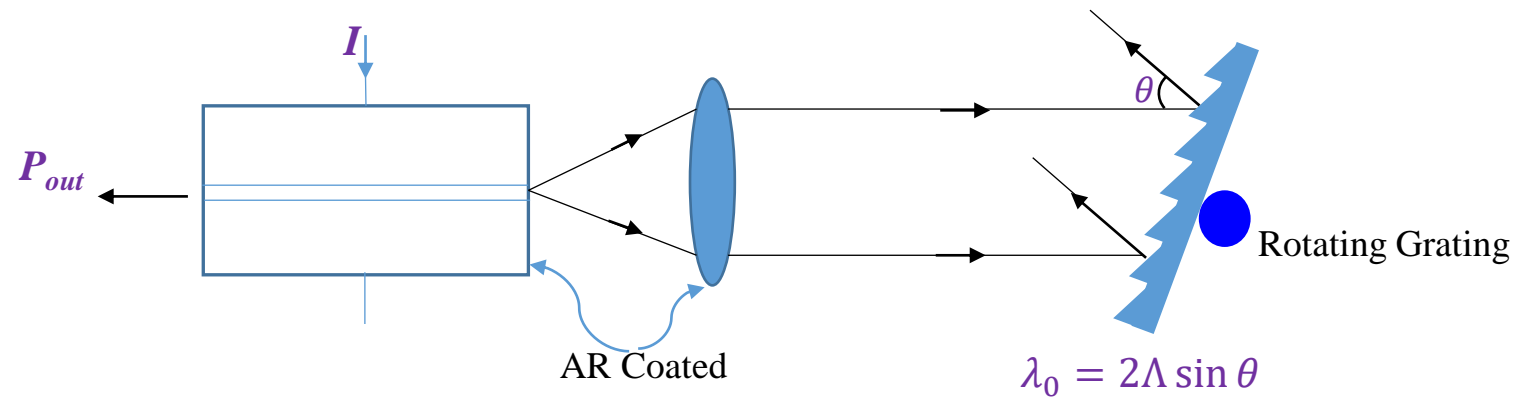
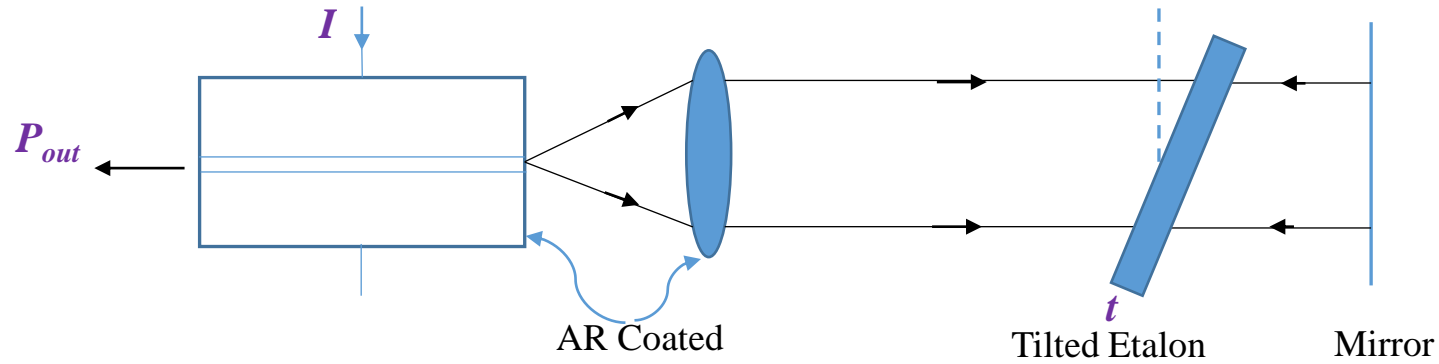
# Output Characteristics: Single Frequency Oscillation

Multi-frequency oscillation leads to large source linewidth



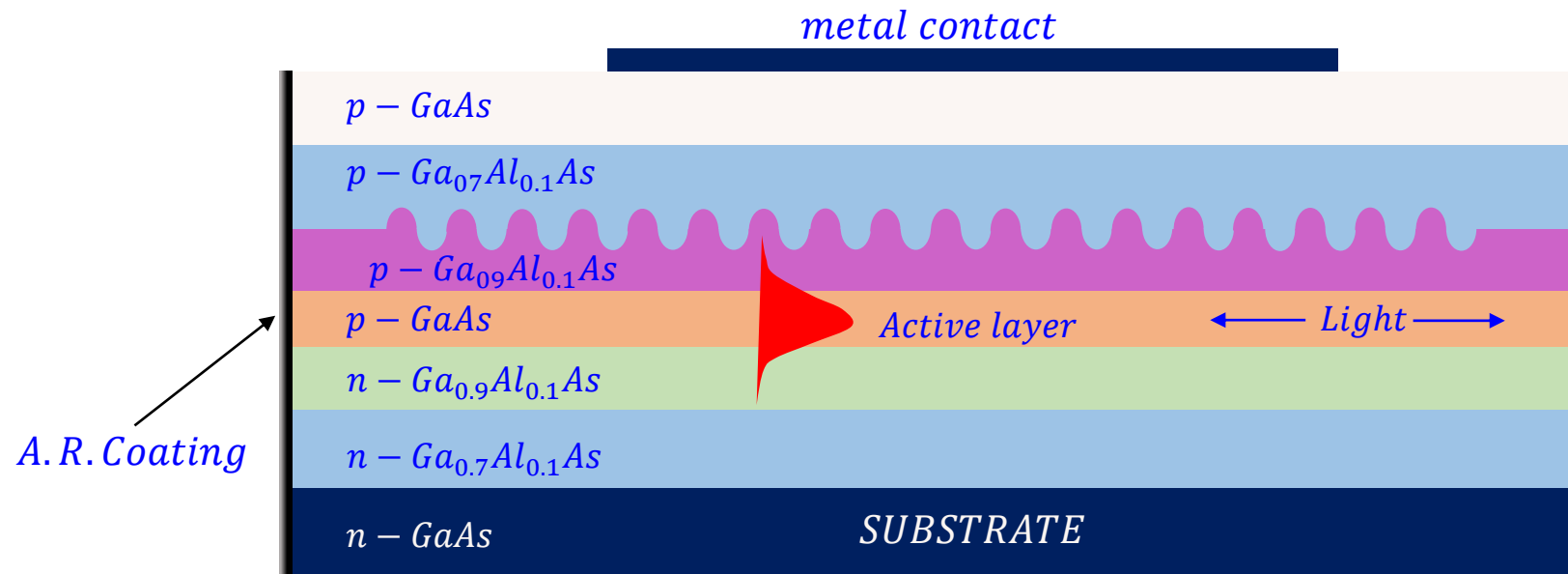
## Why the etalon of small thickness is used?

# Single Frequency Lasers: External cavity



At a given angle, the only one frequency will be selected which satisfy the above equation  
Lossy cavity for other wavelengths  
*Maximum tuning up to 50 nm for ECL*

# Single Frequency Lasers: **DFB Laser**



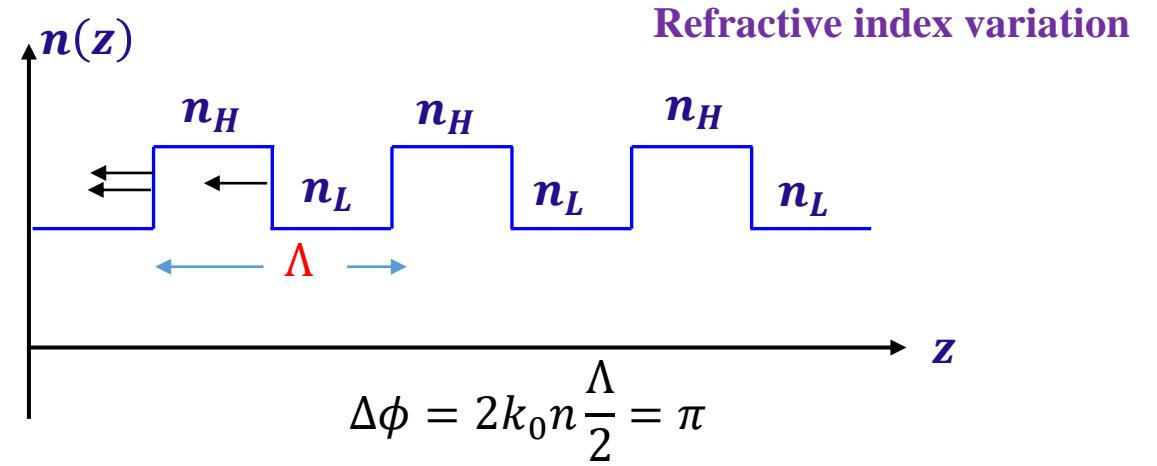
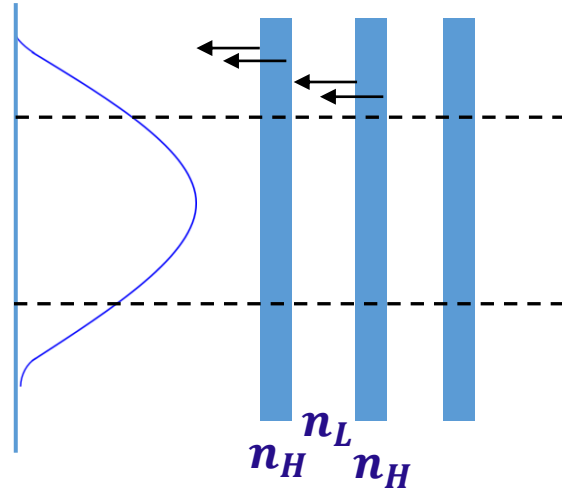
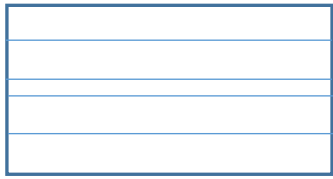
For resonant backward reflection:  $\frac{2\pi}{\lambda_0} n_{eff} 2\Lambda = q \times 2\pi$  ;  $q = 1$  for first order grating

Required grating period:  $\Lambda = \frac{\lambda_0}{n_{eff}}$

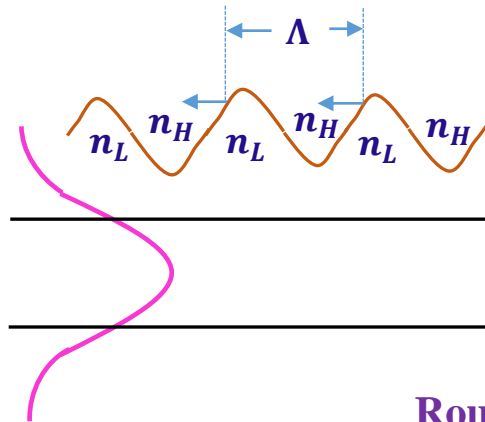
$n_{eff}$ : effective index of the guided mode  $\approx n_{average}$



# Single Frequency Lasers: **DFB Laser**



$$\frac{2\pi}{\lambda_B} n \Lambda = \pi$$



$$2k_0 n_{eff} \Lambda = q \times 2\pi$$

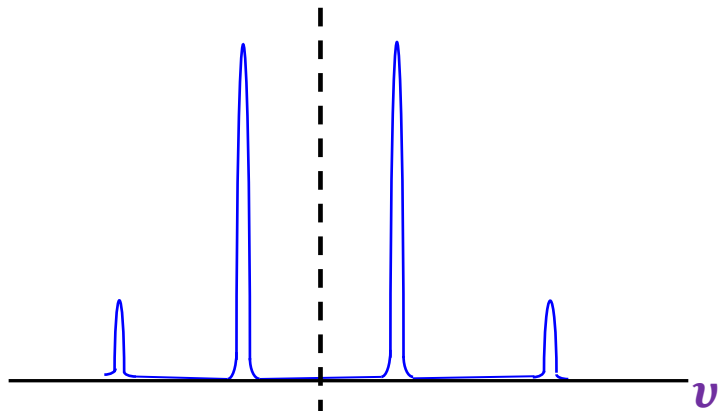
$$\Lambda = \frac{\lambda_0}{2n_{eff}}$$

**For**  $\lambda_B = 1.55 \mu m$

$$\Lambda = \frac{1.55}{2 \times 3.5} \approx 0.23 \mu m$$

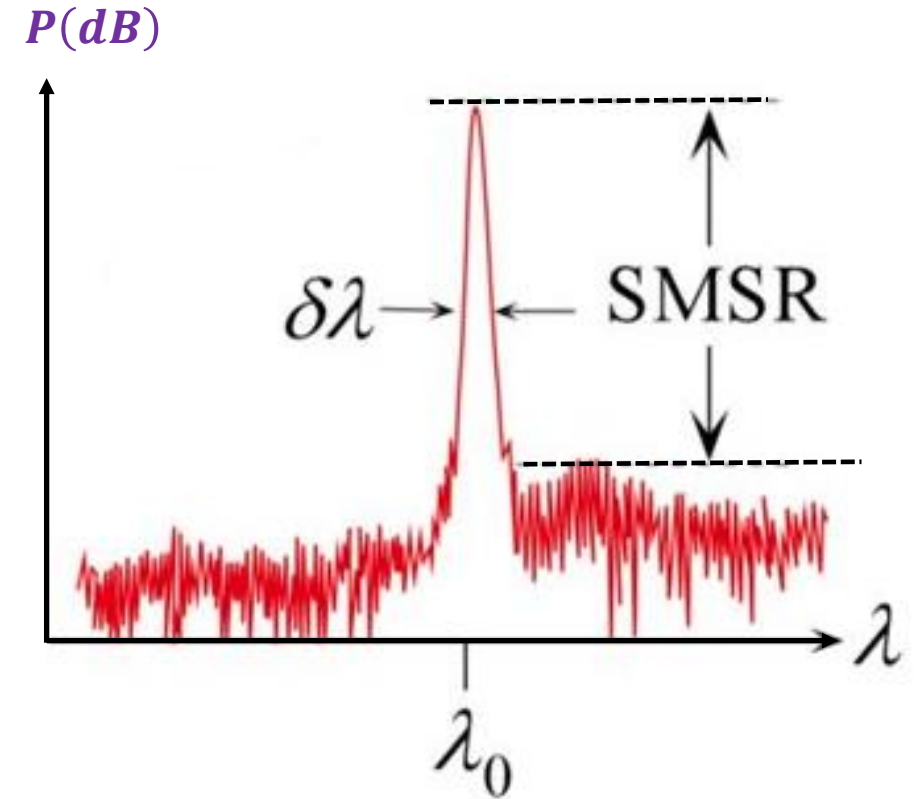
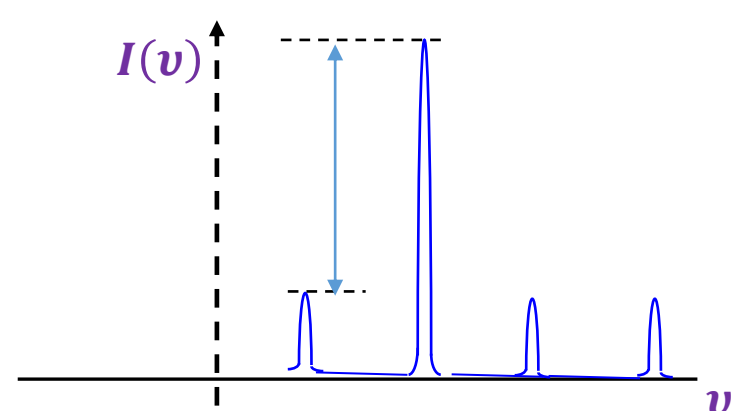
Round trip phase is integral multiple of  $2\pi$ , feedback is only for  $\lambda_0$

# Single Frequency Lasers: **DFB Laser**



$$\nu_B \rightarrow \lambda_B = 2n_{eff}\Lambda$$

$$= \frac{c}{2n_{eff}\Lambda}$$

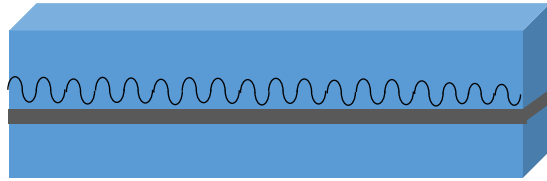


Output spectrum of DFB Laser

But actually the frequency is slightly shift at the laser output

$$\nu_L = \nu_B \pm \left( \frac{c}{2n_{eff}l} \right) \left( q + \frac{1}{2} \right)$$

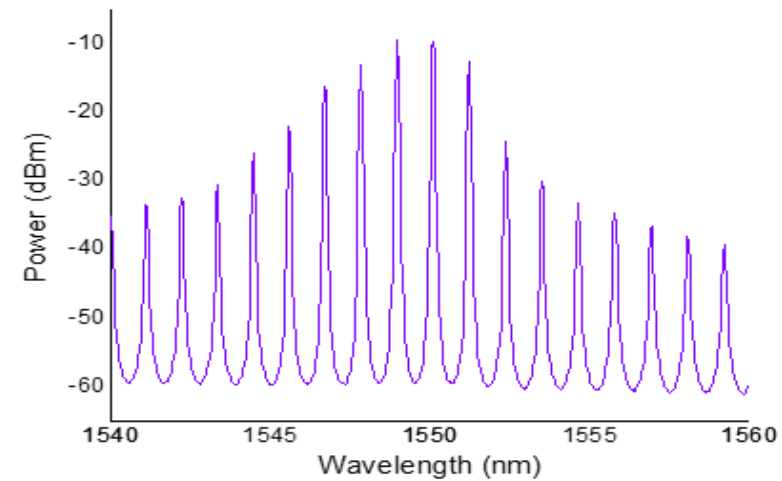
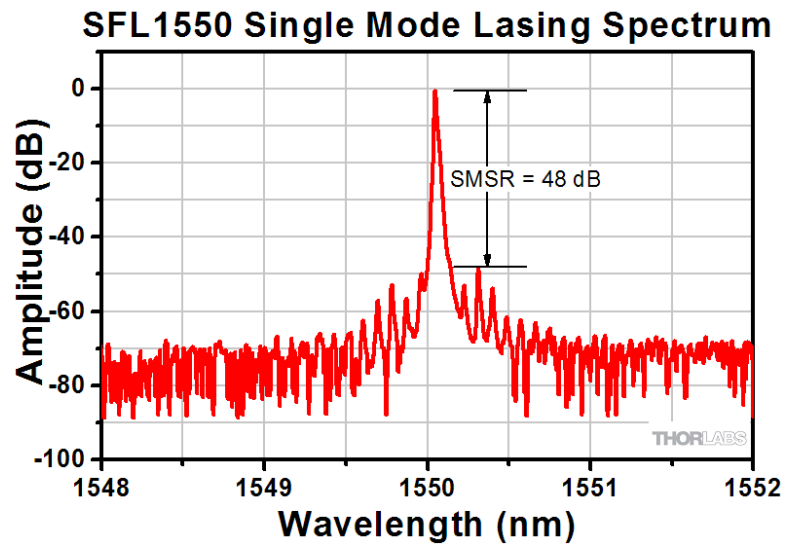
# Single Frequency Lasers: Output Spectrum



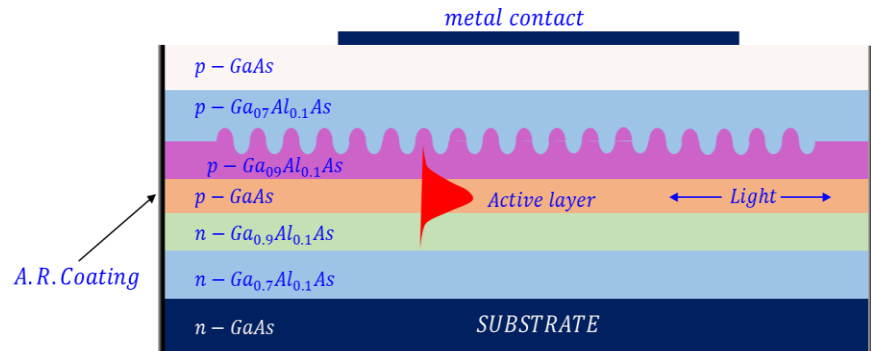
DFB Laser



FP Laser



# Single Frequency Lasers: DBR



DFB Laser



DBR mirror

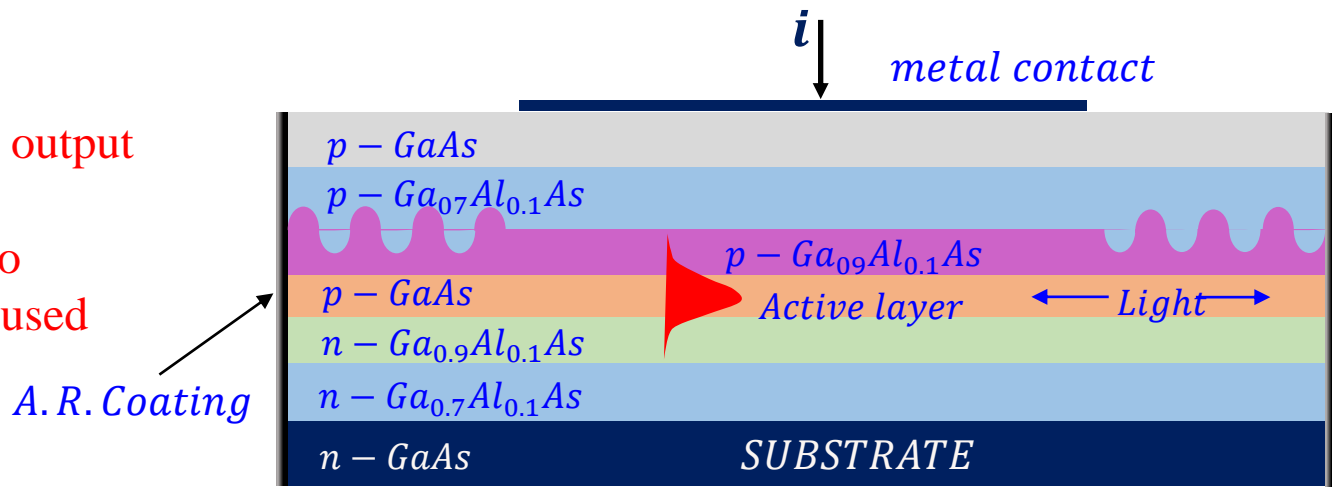
DBR Laser

DBR mirror

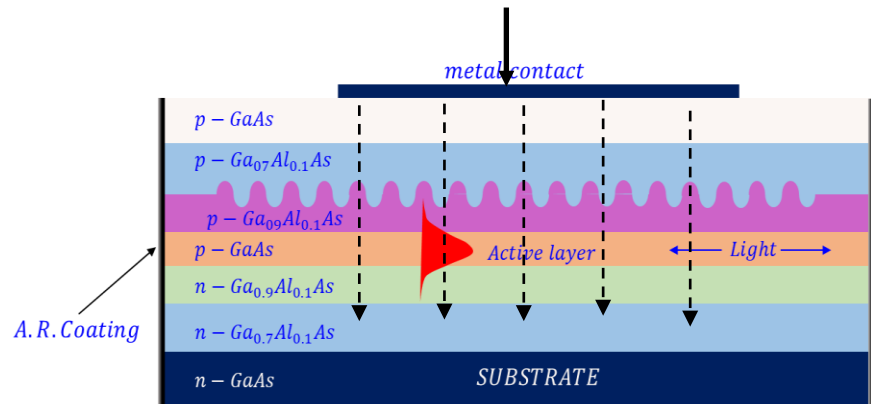


FP Laser

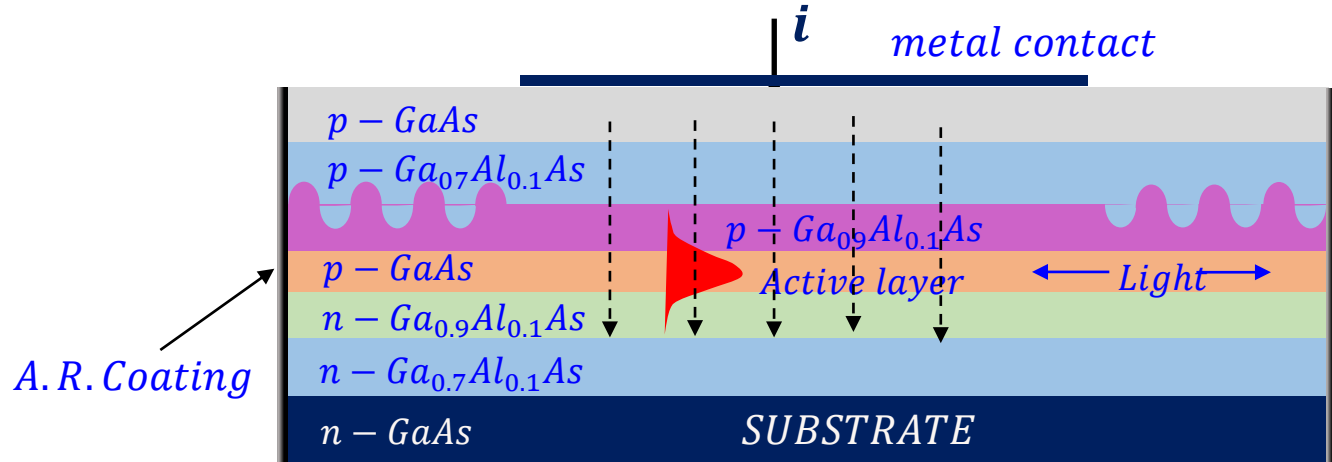
- ❖ More frequency stable at output compared to DFB Laser
- ❖ Comparatively difficult to fabricate DBR mirror so used grating



# Single Frequency Lasers: **DBR**



**DFB Laser**



**DBR Laser**

$$\lambda_b = 2n_{eff}\Lambda$$

- ❖ wavelength fixed when fabricated the corrugation.
- ❖ However refractive index of the medium  $n_{eff}$  which is depend on the injection current.
- ❖ Depending upon the energy level difference greater and lesser than  $E_g$  which determines whether the active medium acts as gain or absorber.

Plane wave :  $\psi = Ae^{i(\omega t - kz)}$  ;  $k = k_0 n$   
 $= Ae^{i\omega t} e^{-ik_0 n_r z} e^{-k_0 n_i z}$

$$n = n_r - in_i$$

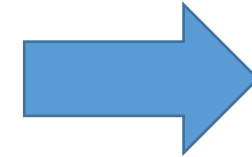
$n_i > 0 \rightarrow$  Absorbing  
 $n_i < 0 \rightarrow$  Gain

$$I = |\psi|^2 = A^2 e^{-2k_0 n_i z}$$

$$I(z) = |\psi|^2 = I_0 e^{-2k_0 n_i z}$$

# QUIZ # 1

**Why are the end facets of a DFB laser chip provided with AR coating**

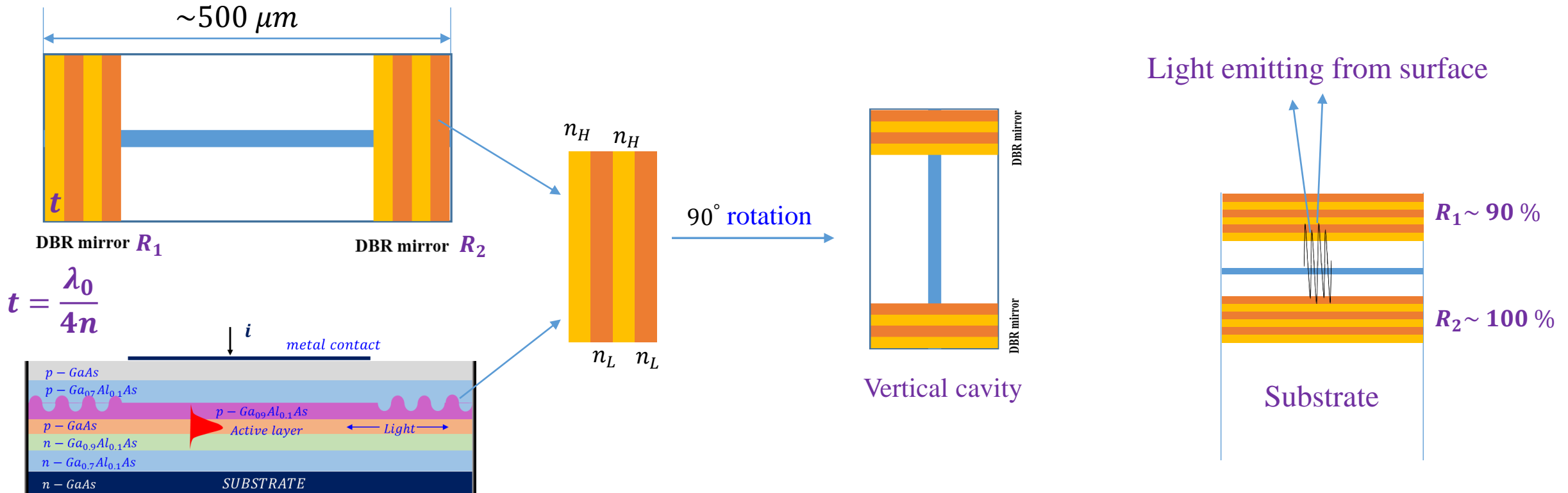


# Answer of Quiz # 1

**To prevent reflections from the end facets that could lead to the formation of Fabry-Perot cavity/resonances.**

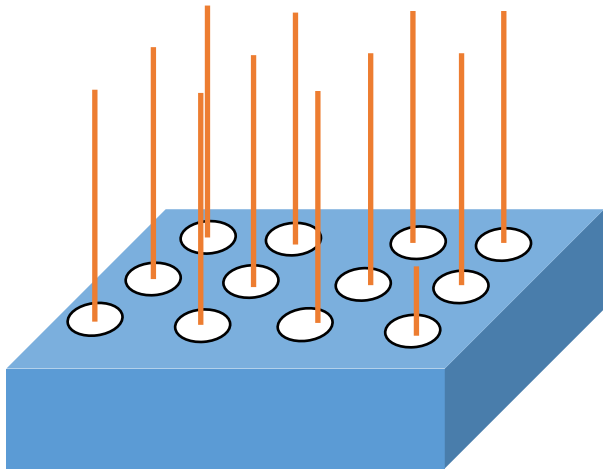
# Single Frequency Lasers: VCSELs

Vertical Cavity Surface Emitting Laser, VCSELs → Variation of DBR Laser





# Single Frequency Lasers: VCSELs



Use for High density data interconnects in computer design

For Example:

For equilibrium for resonator

$$\alpha_r = \gamma = \alpha_s + \alpha_m$$

$$\gamma = 50 \text{ cm}^{-1}$$

$$\alpha_s = 10 \sim 50 \text{ cm}^{-1}$$

For minimum values of  $\alpha_s$

$$\begin{aligned} \alpha_m &= 40 \text{ cm}^{-1} \\ &= \frac{1}{2l} \ln \left( \frac{1}{R_1 R_2} \right) \end{aligned}$$

$$\therefore l = \frac{1}{2\alpha_m} \ln \left( \frac{1}{R_1 R_2} \right)$$

For normal laser diodes

$$R_1 = R_2 \sim 32\% \text{ lower percentage}$$

For VCSELs and DBR

$$R_1 = R_2 \geq 90\% \text{ higher value}$$

For  $R_1 = R_2 = R$

$$\therefore l = \frac{1}{40} \ln \left( \frac{1}{R} \right)$$

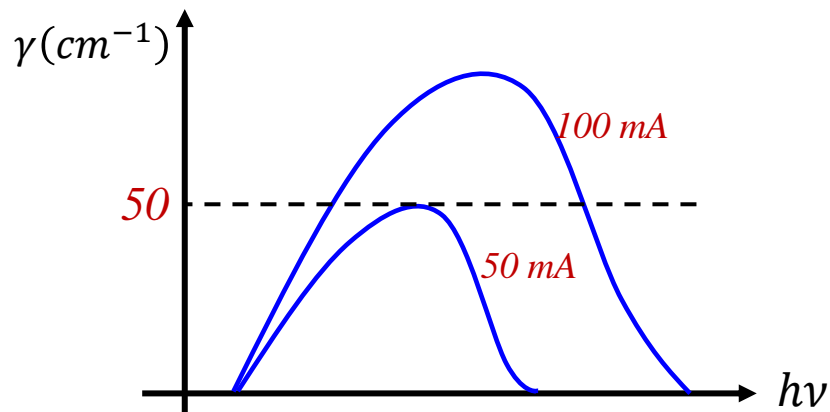
For different values of  $R$

$$R=0.32 \longrightarrow l \approx 285 \mu\text{m}$$

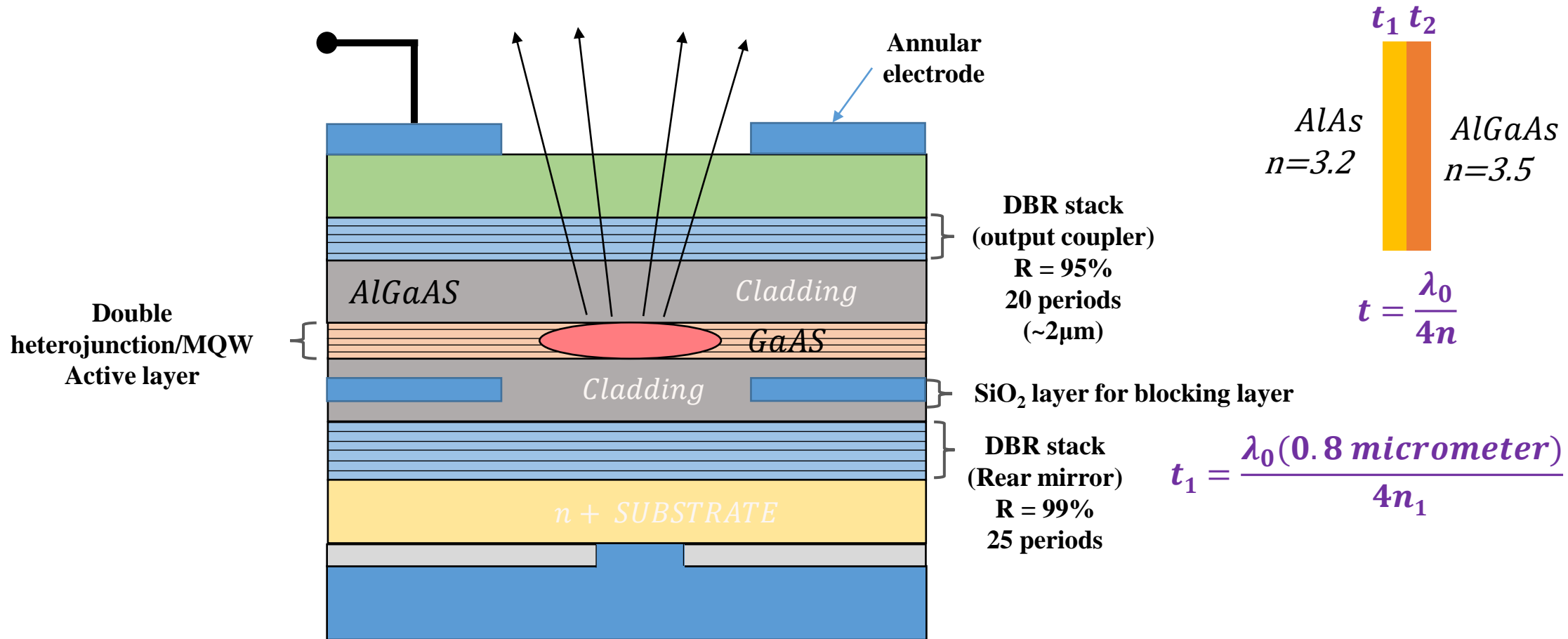
$$R=0.9 \longrightarrow l \approx 10 \mu\text{m}$$

$$R=0.99 \longrightarrow l \approx 2.5 \mu\text{m}$$

$$R=0.998 \longrightarrow l \approx 0.2 \mu\text{m}$$



# Single Frequency Lasers: VCSELs



Vertical cross section of a VCSEL

# Single Frequency Lasers: Bragg Reflectors

$$\alpha_r = \alpha_s + \alpha_m \Rightarrow \gamma_p$$

$10 \text{ cm}^{-1}$        $40 \text{ cm}^{-1}$        $50 \text{ cm}^{-1}$

For different values of R

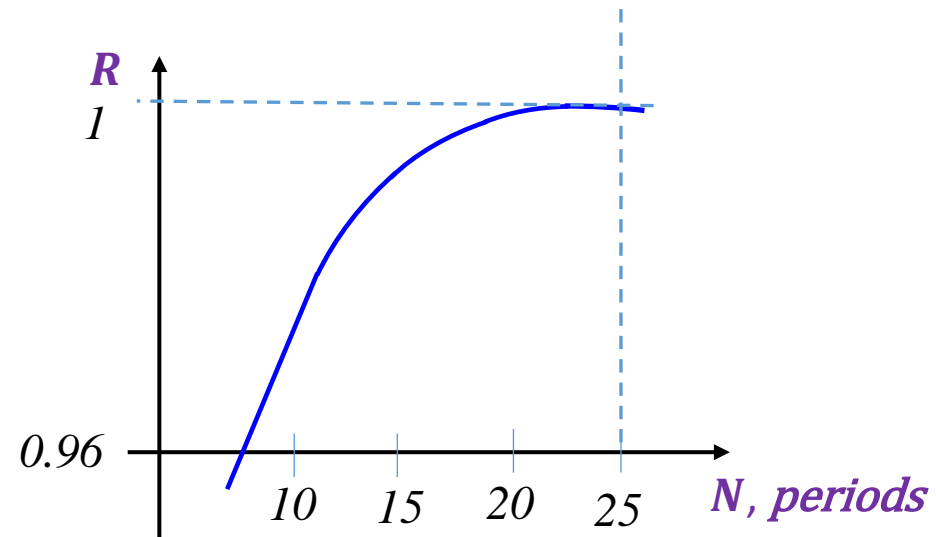
$R=0.32 \longrightarrow l \approx 285 \mu\text{m}$

$R=0.9 \longrightarrow l \approx 10 \mu\text{m}$

$R=0.998 \longrightarrow l \approx 0.2 \mu\text{m}$

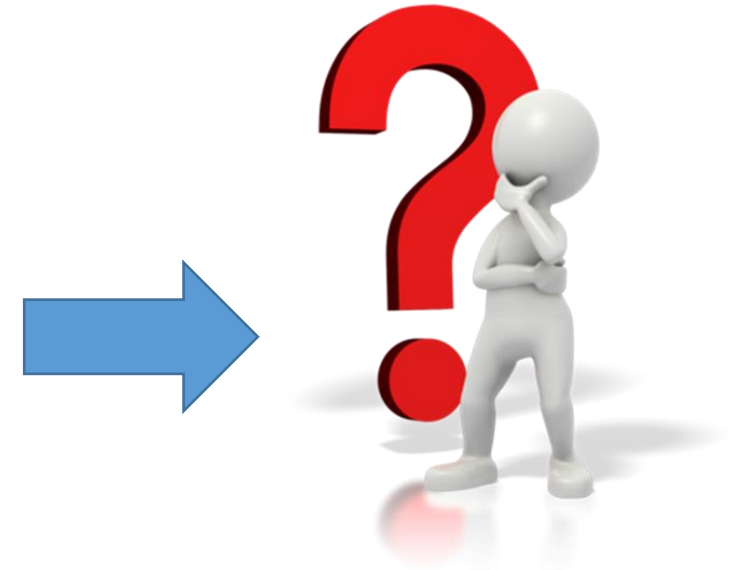
Reflectivity of a periodic stack of “high” and “low” index layer is given by

$$R = \left[ \frac{1 - \left(\frac{n_L}{n_H}\right)^{2N}}{1 + \left(\frac{n_L}{n_H}\right)^{2N}} \right]^2$$



# QUIZ # 2

**Why VCSELs have only a single wavelength and greater FSR?**



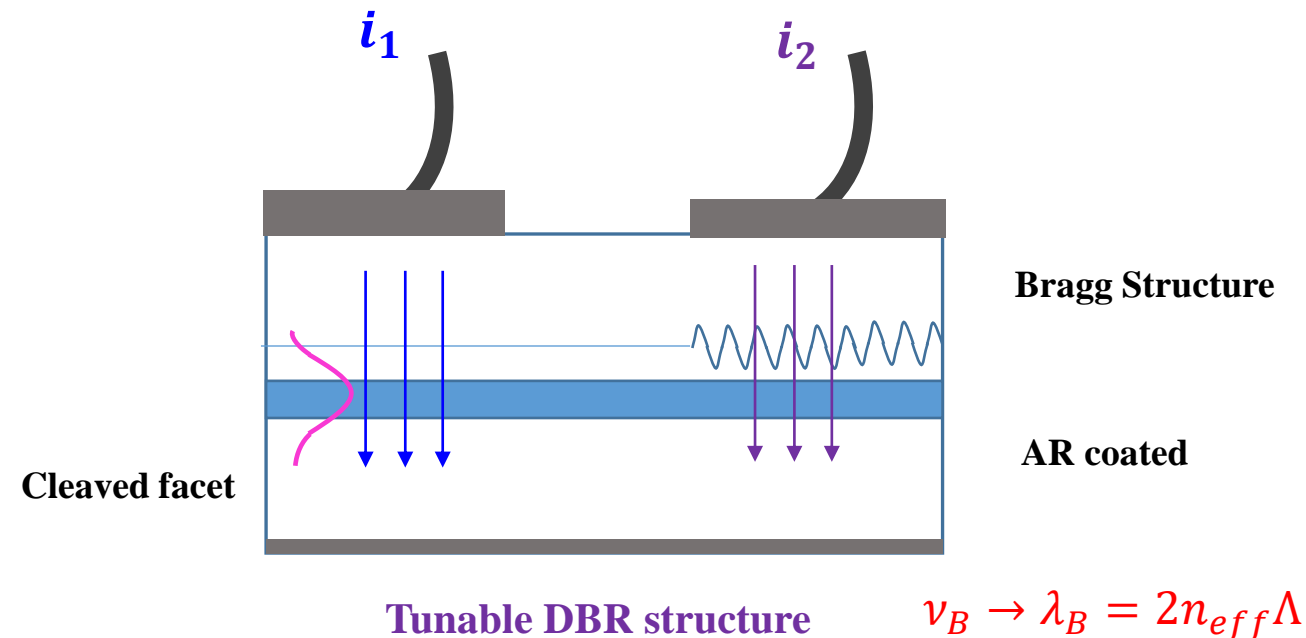
# Answer of Quiz # 2

**Due to Bragg stacks  
Cavity length is small**

In VCSELs the cavity length is about  $10\ \mu\text{m}$  hence FSR is large and normally the bandwidth of the amplifier cannot cover the more than one longitudinal mode and hence most of the cases VCSELs are SM lasers.

# Single Frequency Lasers: Tunable DBR

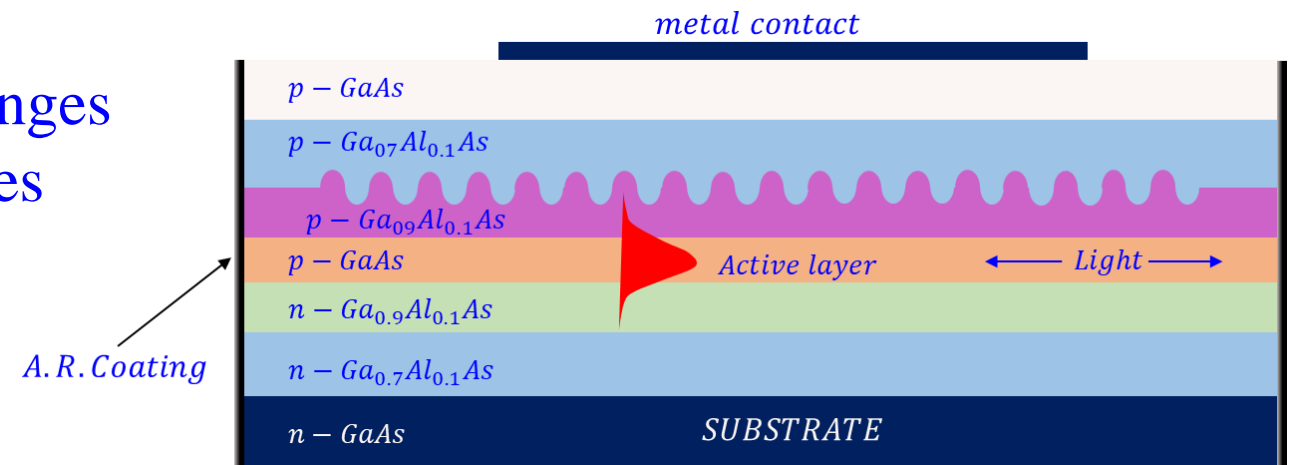
- ❖ two section structure
- ❖ Biased separately for two structure
- ❖ Frequency selection due to change in Refractive index and Bragg grating frequency
- ❖ Tuning range is from 5 nm to 10 nm



$$\nu_B \rightarrow \lambda_B = \frac{2n_{eff}\Lambda}{c}$$

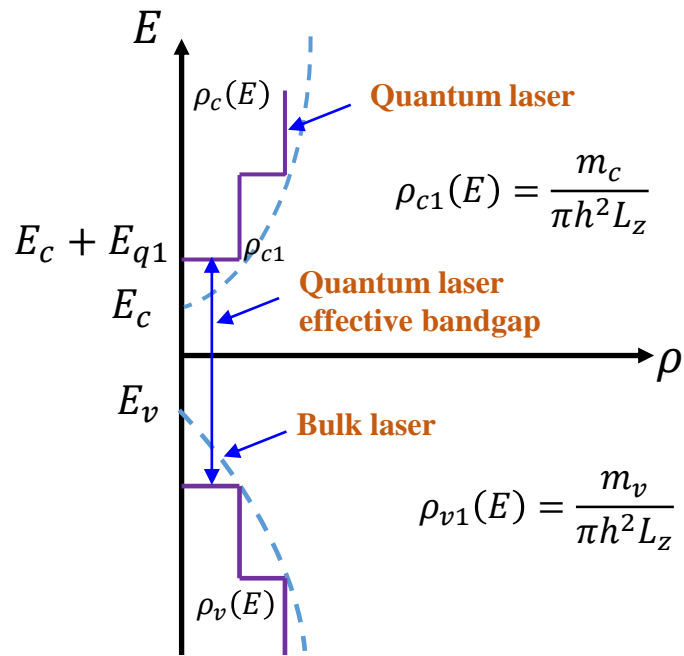
# Single Frequency Lasers: Tunable DFB

- ❖ Change in Temperature : bandgap changes and hence emitting wavelength changes
- ❖ Only small tunable range of 1~3 nm
- ❖  $\Delta\lambda = 0.1\text{nm}/\text{oC}$

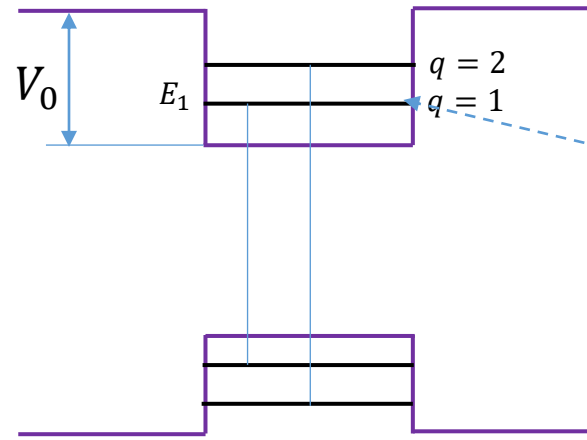


# Single Frequency Lasers: Quantum Well Lasers

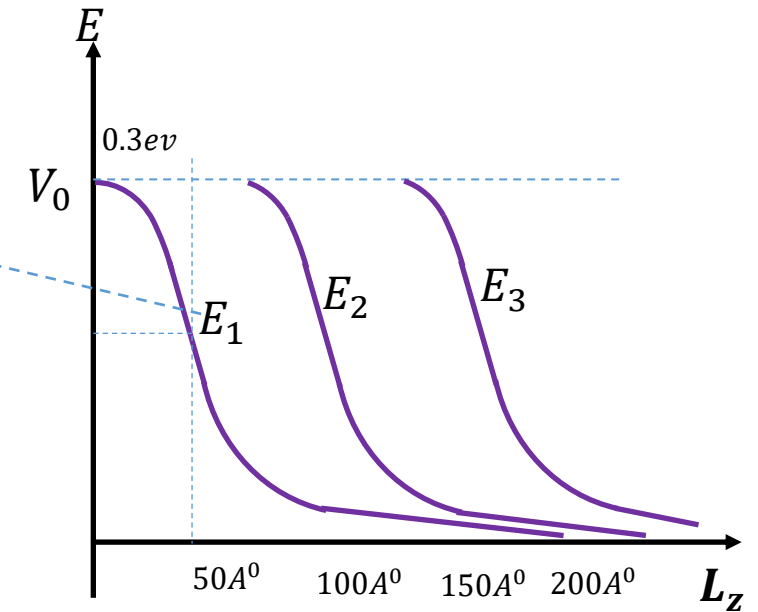
Most of the Lasers have the Quantum Well in Active region



Density of states in Quantum well structures



Energy states in Quantum well structures

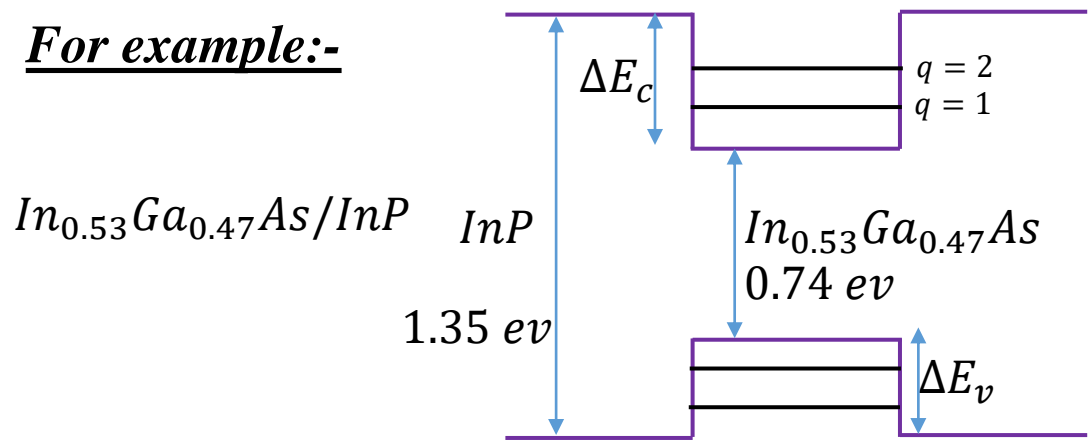


Allowed energy values for different quantum well energy number with quantum well thickness



# Single Frequency Lasers: Quantum Well Lasers

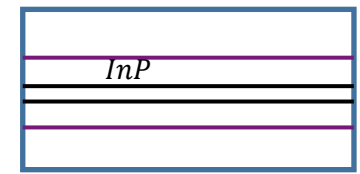
For example:-



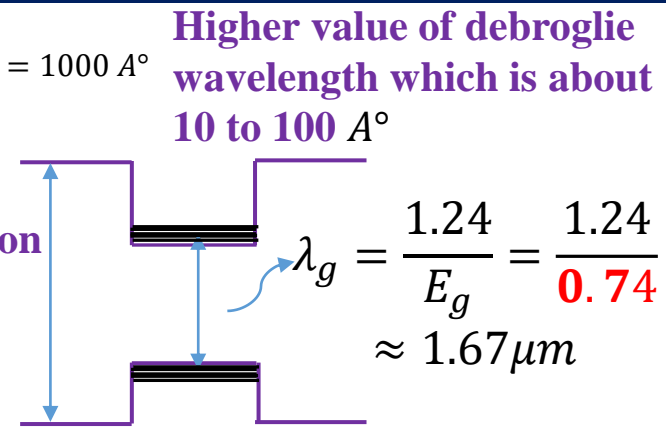
$$\Delta E_g = 0.61 \text{ eV}$$

$$\Delta E_c \approx 0.65 \Delta E_g \approx 0.4 \text{ eV}$$

$$\Delta E_v \approx 0.35 \Delta E_g \approx 0.21 \text{ eV}$$



Double heterostructure

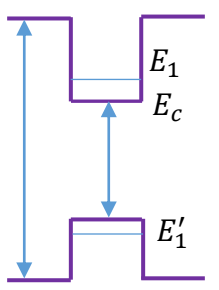


Higher value of de Broglie wavelength which is about 10 to 100 Å

$$\lambda_g = \frac{1.24}{E_g} = \frac{1.24}{0.74} \approx 1.67 \mu\text{m}$$

When d is changed to 100 Å

Typical value



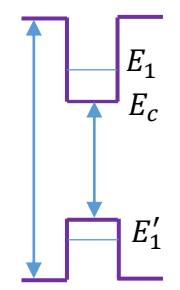
$$\Delta E_1 = E_c - E_1 \approx 50 \text{ meV}$$

$$\Delta E'_1 \approx 10 \text{ meV}$$

$$E_g^{eff} = 0.74 + 0.05 + 0.01 = 0.8$$

$$\lambda_g = \frac{1.24}{E_g} = \frac{1.24}{0.8} \approx 1.55 \mu\text{m}$$

Further decrease to 80 Å



$$\Delta E_1 \approx 85 \text{ meV}$$

$$\Delta E'_1 \approx 15 \text{ meV}$$

$$E_g^{eff} = 0.74 + 0.085 + 0.015 = 0.84$$

$$\lambda_g = \frac{1.24}{E_g} = \frac{1.24}{0.84} \approx 1.46 \mu\text{m}$$

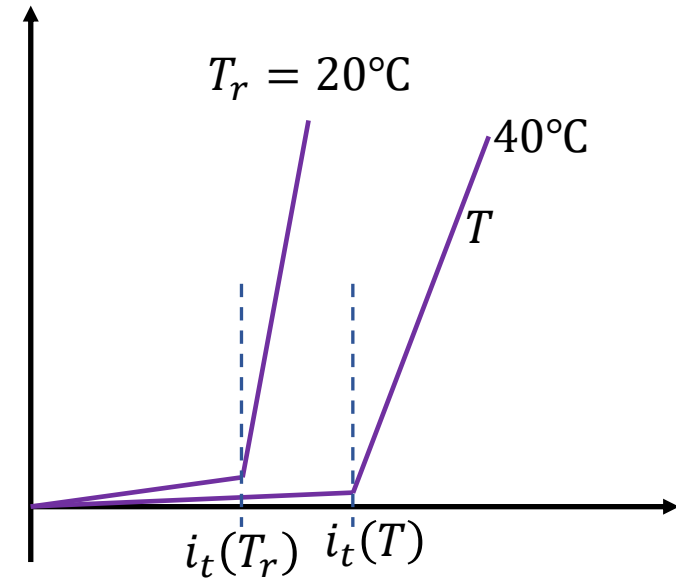
change in small width with change in higher emission of wavelength

# Single Frequency Lasers: Quantum Well Lasers

Semiconductor laser double heterojunction laser, where the thickness of active layer is less than de Broglie wavelength of electrons (200 Å to 5 nm which give quantization and gives discrete level of energy)

- ❖ Lower threshold
- ❖ Less sensitive to temperature variation
  - $T_0 \sim 140 \text{ K}$  for FP lasers
  - $T_0 \sim 400 \text{ K}$  for QW lasers

$$i_t(T) = i_t(T_r) e^{\left(\frac{T-T_r}{T_0}\right)}$$



larger the value of  $T_0$  less shift in temperature

- ❖ Carrier distribution is less sensitive to the temperature due to the transition level need to be changed as **discrete energy level** unlike the bulk lasers
- ❖ In QW lasers with increase in temperature there is less non radiative transition hence quantum efficiency,  $\eta_i$  is relatively large and quantum efficiency is less effective with temperature

# Single Frequency Lasers: Quantum Well Lasers

Gain coefficient

$$\gamma = \alpha_a \left( \frac{\Delta n}{\Delta n_T} - 1 \right) = \alpha_a \left( \frac{J}{J_T} - 1 \right)$$

$$\gamma = \frac{\lambda^2}{8\pi\tau} \rho(\nu) f_g(\nu)$$

Density of states in Quantum well structures

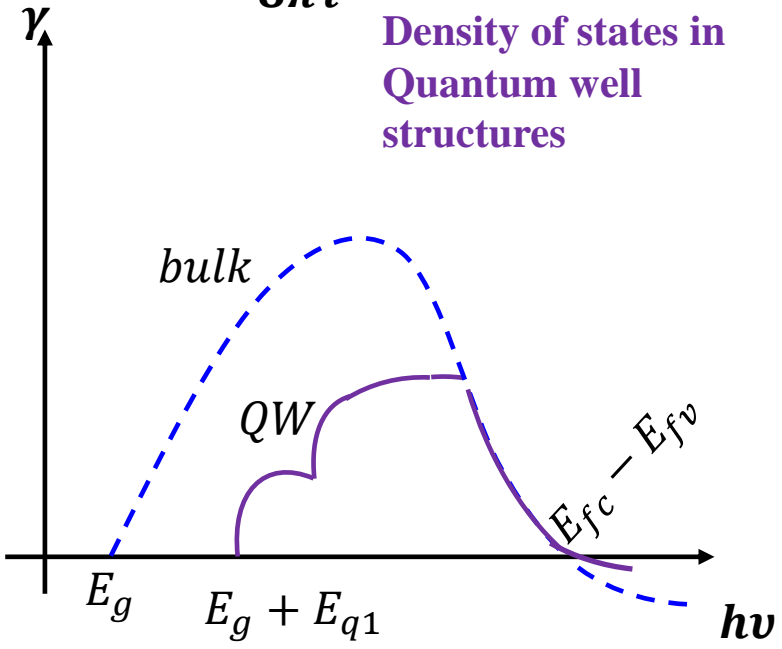


Fig. 1 Gain as a function of Energy

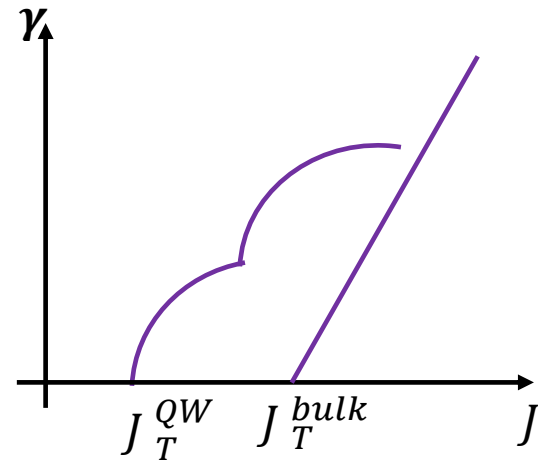
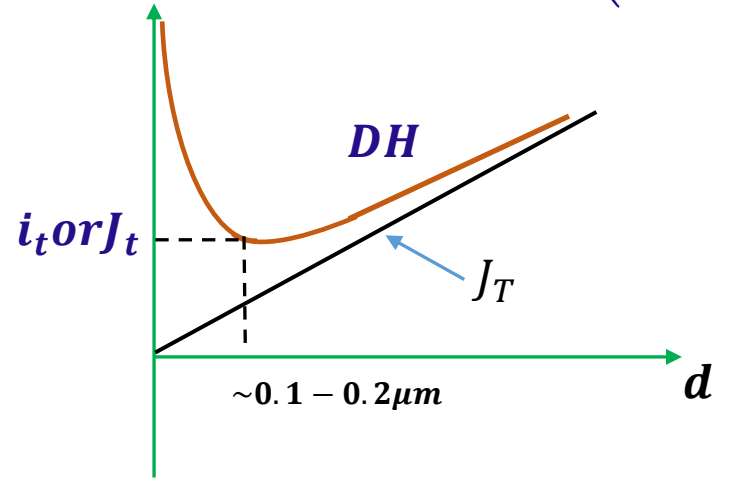


Fig. 2 Gain as a function of current density

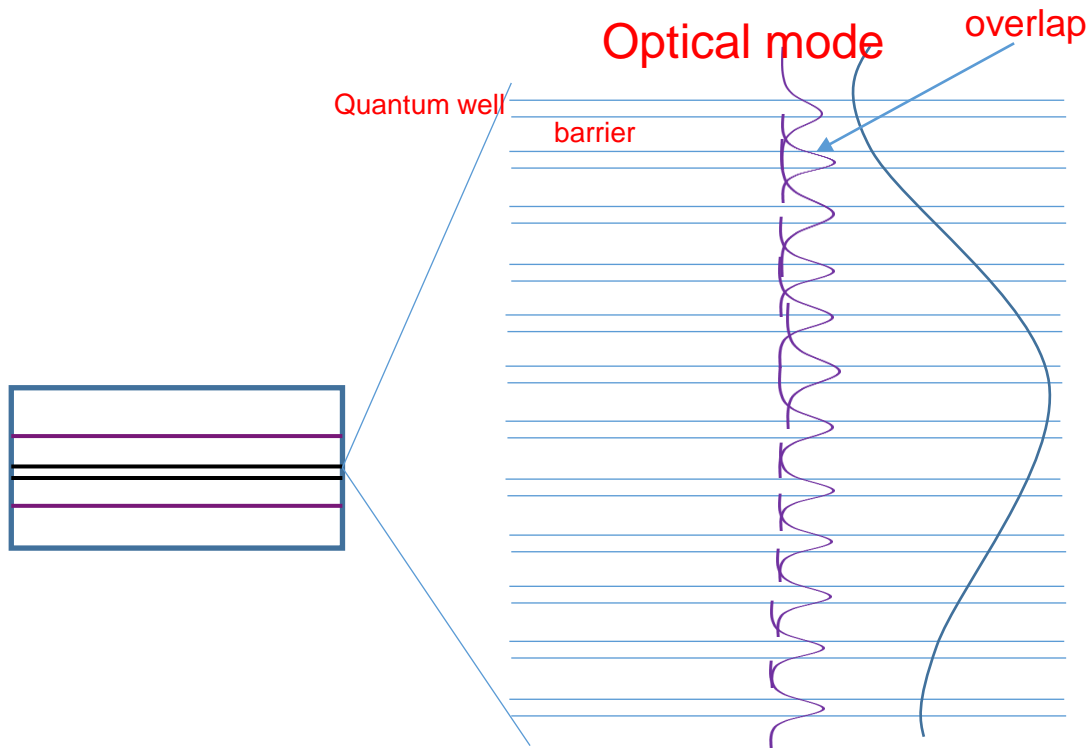
Confinement factor:  $J_t = J_T \left( 1 + \frac{\alpha_r}{\Gamma \alpha_a} \right)$



For QW lasers

- ❖ d is less then we expect threshold to go which is because of confinement factor  $\Gamma$  in heterojunction
- ❖ In QW lasers although the confinement factor is small gain is much higher for QW well and quantum efficiency is very high and  $f_g(\nu)$  increase rapidly
- ❖ Net effect even we have less value of d, less the threshold current

# Single Frequency Lasers: MQW



## MQW lasers

- ❖ Active level comprises of multiple quantum well structures comprises of identical potential wells and barriers.
- ❖ Barrier thickness is sufficiently large so that electron wave function does not interact with each other.
- ❖ Identical not interacting wells
- ❖ Enhancement of effective gamma with one overall optical field
- ❖ Higher optical output power as overall active area increases
- ❖ Typical 2 to 6 QW layer

# Assignment# 03

1. Why DBR laser have better frequency stability compared to the DFB laser?
2. Why the reflectivity  $R$  is chosen higher value in VCSELs?
3. Why the coupling efficiency of VCSELs is better than Fabry perot lasers?

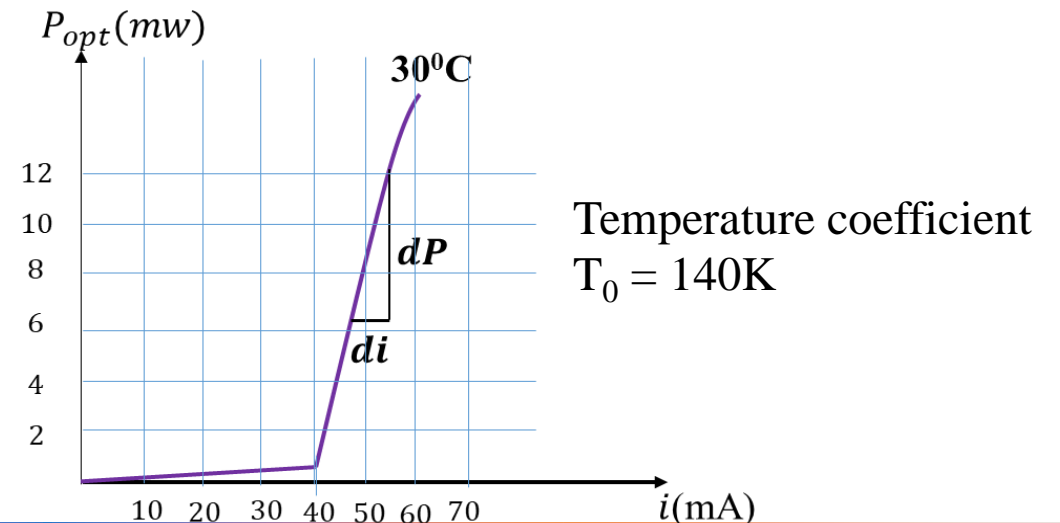
4. For the given typical parameter of laser diode as follows, what is the transparent current at  $T=30^{\circ}\text{C}$  and  $T=40^{\circ}\text{C}$ . Also, plot the graph for  $P_{\text{optical}}$  when the temperature is raised to  $40^{\circ}\text{C}$  showing threshold current.

Scattering loss due to inhomogeneity =  $20\text{ cm}^{-1}$ ;

Absorption co-efficient =  $600\text{ cm}^{-1}$ ;

Length of the cavity =  $285\text{ }\mu\text{m}$ ;

Reflectivity of cavity mirrors are 32%



**Any Queries**

